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## Exploration of artificial multiferroic thin-film heterostructures using composition spreads

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We have fabricated a series of composition spreads consisting of ferroelectric  $BaTiO_3$  and piezomagnetic  $CoFe_2O_4$  layers of varying thicknesses modulated at nanometer level in order to explore artificial magnetoelectric thin-film heterostructures. Scanning microwave microscopy and scanning superconducting quantum interference device microscopy were used to map the dielectric and magnetic properties as a function of continuously changing average composition across the spreads, respectively. Compositions in the middle of the spreads were found to exhibit ferromagnetism while displaying a dielectric constant as high as  $\approx 120$ . © 2004 American Institute of Physics. [DOI: 10.1063/1.1699474]

Magnetoelectric materials<sup>1</sup> are one class of multiferroics in which charge polarization and magnetization coexist and are coupled together. Such materials can display a magnetoelectric effect in which change in magnetization is induced by an electric field and change in electric polarization is induced by an applied magnetic field. This property can be used as a basis for novel actuators and sensors with high sensitivity.<sup>2</sup> Van Suchtelen and co-workers<sup>3-5</sup> made the first artificial magnetoelectric material by combining a ferroelectric (piezoelectric) material BaTiO<sub>3</sub> (BTO) and a ferromagnetic (piezomagnetic) material CoFe<sub>2</sub>O<sub>4</sub> (CFO) in an eutectic sintered composite. There have also been reports of magnetoelectric effects in layered composites such  $(Pb,Zr)TiO_3 (PZT)-Tb_{0.3}Dy_{0.7}Fe_{1.92}$ (Terfenol-D), PZT-NiFeO<sub>4</sub>, polyvinylidenefluoride-Terfenol-D and laminate Pb(Mg<sub>1/3</sub>Nb<sub>2/3</sub>)O<sub>3</sub>-PbTiO<sub>3</sub>-Terfenol-D.<sup>6-9</sup>

To date, these composite materials have been exclusively studied in bulk materials. The present work explores the possibility of fabricating such materials in a thin-film form. Thin-film samples have several advantages over bulk samples: (1) magnetoelectric thin-film heterostructures can be constructed by alternating piezoelectric and piezomagnetic layers, and one can investigate coupling of the two properties at nanometer levels; and (2) one can pursue fabrication of compact thin-film magnetoelectric devices. Our initial goal is to create materials that are simultaneously ferroelectric and ferromagnetic. We explore this by fabricating structures in which ferroelectric and ferromagnetic layers alternate with nanometer-thick periods. In constructing such structures, there are many parameters to be optimized: compositions, thickness of each layer, etc. In order to rapidly

magnetic materials, respectively.

(a)

FIG. 1. (a) The schematic of the composition spreads. (b) Synthesis scheme of the spread. The thickness of each wedge can be varied from less than one unit cell to multiples of unit cells at the thick end. The total thickness is 300 nm everywhere.

map the parameter space, we implement the continuous com-

position spread approach. In particular, we use a design of

the spread in which one end of the spread is a pure piezoelectric material and the other end is a pure piezomagnetic

material, and they are gradually mixed together toward the

center of the spread. This technique allows us to systematically investigate mixing and changing of the two physical

properties as a function of average composition, which con-

tinuously varies across the spread (Fig. 1). The magnetoelec-

tric coefficient has been reported to be a function of the ratio of the volume of the piezoelectric phase to the volume of the

piezomagnetic phase in bilayered or multilayered

structures. 10-12 The present composition spread technique

can offer an efficient way to systematically optimize the vol-

ume ratio to obtain the maximum magnetoelectric effect.

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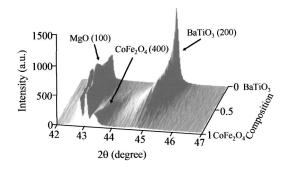


FIG. 2. The scanning x-ray microdiffraction of the spread sample, for which t is 1.68 nm. The intensity is plotted as a function of  $2\theta$  (from  $42^{\circ}$  to  $47^{\circ}$ ) and as a function of average composition (from pure BTO to pure CFO).

Previously, we have fabricated high-quality composition spreads of  $(Ba_x, Sr_{1-x})TiO_3$ . Unlike these previous studies, BTO and CFO do not form solid solutions, and thus, in order to provide some "integrity" in the respective materials, spreads were made in such a way that there is more than one unit cell of BTO and CFO at the thick end of each wedge layer (henceforth defined as t). We made a series of composition spreads in which t was approximately 0.84, 2.52, 8.4, and 12.6 nm [see Fig. 1(b)]. These numbers roughly correspond to  $1\times$ ,  $3\times$ ,  $10\times$ , and  $15\times$  the unit cell of CFO. BTO has a pseudocubic structure with the lattice constant a = 0.403 nm, and CFO has a spinel cubic structure with the lattice constant a=0.839 nm. Although the two materials have different structures, the mismatch between twice the lattice parameter of BTO and that of CFO is roughly 5%, and we have found that they can be grown together in a heteroepitaxial manner on (100) MgO (cubic with a = 0.42 nm). The oxygen partial pressure during the deposition was 65 mTorr, and the substrate was held at the temperature of 800 °C. The typical size and the thickness of a composition spread sample was 6 mm (in the spread direction)×10 mm and 300 nm (uniform across spreads), respectively. In each spread, the average composition continuously changes from pure BTO to pure CFO.

Structural changes of the BTO-CFO artificial multilayers across the spreads were studied by the  $\omega$ -scan mode of a scanning x-ray microdiffractometer (D8 DISCOVER with GADDS for combinatorial screening by Brucker-AXS). A 300  $\mu$ m spot size was used to take 20 points across each spread. The x-ray intensity as a function of  $2\theta$  and of the average composition for a spread in the  $2\theta$  range of  $42^{\circ}$  to  $47^{\circ}$  is shown in Fig. 2. The peaks are integrated from  $-94.9^{\circ}$  $<\chi<-78.4^{\circ}$ . t was approximately 1.7 nm for this sample. It is seen that the (200) BTO peak and the (400) CFO peak continuously "evolve" toward the middle of the spread. The continuous shifts and the broadening of the peaks are indicative of significant and progressive lattice distortion caused by diffusion of cations (Ba2+ and Ti4+ of BTO and Co2+ and Fe<sup>3+</sup> of CFO) at the multilayer interfaces. We have found that there is less lattice distortion toward the middle of the spread for spreads with larger thickness of the wedge layers; the x-ray peak positions do not shift in the middle of the spread for samples in which t is  $10 \times$  and  $15 \times$  the unit cell of CFO. This is consistent with the fact that in comparing spreads with different wedge thicknesses, there are fewer interfaces when the individual layer is thicker, and thus there

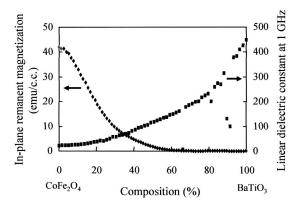


FIG. 3. Dielectric constant (right) measured by the microwave microscope, and the in-plane remanent magnetization (left), characterized by the scanning SQUID microscope as a function of average composition across the spread. *t* for this spread is 8.4 nm.

is a smaller overall fraction of materials affected by the interdiffusion at the interfaces.

In order to study the continuously changing properties of the spreads, microwave microscopy<sup>13</sup> and room-temperature scanning superconducting quantum interference device (SQUID) microscopy were used. The linear dielectric constant measured at 1 GHz using the microwave microscope is shown in Fig. 3 for a spread in which t was 8.4 nm. The linear dielectric constant systematically decreases from 450 for the pure BTO end to 40 for the pure CFO end. The decreasing trend across the spread was found to be similar for all spreads, and the general trend is consistent with the one obtained from calculating the effective dielectric constant using the series capacitance model, in which layers with different dielectric constants are alternating. Comparing different spreads, we found that the dielectric constant at the same average composition is higher for the spreads with thicker wedge layers, consistent with the fact that thicker individual layers would have better overall materials integrity, as discussed earlier. This trend is evident in Fig. 4 for a dielectric constant measured at the average composition of  $(BTO)_{0.45}$  –  $(CFO)_{0.55}$  for spreads with different wedge layer thicknesses. This trend may also be related to the ferroelectric size effect in thin films. 14,15 The dielectric loss value at 1 GHz was found to vary continuously from ≈0.2 for the BTO end to  $\approx 0.3$  for the CFO end for all the spreads. These loss values are comparable to values obtained by other measure-

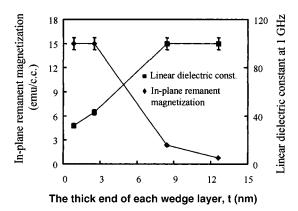


FIG. 4. Dielectric constant (right) and in-plane remanent magnetization (left) at the average composition  $(BTO)_{0.45}$ – $(CFO)_{0.55}$  from a series of composition spreads.

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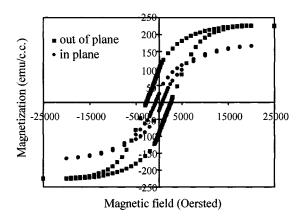


FIG. 5. A SQUID magnetometer measurement of M-H curves of a single composition sample of  $(BTO)_{0.45}-(CFO)_{0.55}$ . The periods of CFO and BTO layers are  $\approx 1.4$  nm and  $\approx 1.1$  nm, respectively.

ment methods for epitaxial (Ba,Sr)TiO<sub>3</sub> films at microwave frequencies. <sup>16,17</sup>

In order to characterize the ferromagnetic properties, mapping of magnetic field emanating from the sample due to remanent magnetization is obtained using a roomtemperature scanning SQUID microscope. We magnetize our samples in the in-plane direction, even though the films studied here predominately showed the out-of-plane direction as the easy axis. This is because our present algorithm<sup>18</sup> for obtaining quantitative remanent magnetization uses an inplane magnetized model. The trend of how the in-plane remanent magnetization changes as a function of various parameters is used as an indicator of the overall magnetic properties. Comparing the in-plane remanent magnetization of the series of composition spreads at the same average composition, the spreads with thinner layer thicknesses seem to sustain higher remanent magnetization (as seen in Fig. 4). This could be explained by the mismatch stresses or strains between ferrite films and substrates, inducing enhanced magnetization for thinner layers. 19,20 Despite the decaying of properties as one goes toward the middle of the spread, we see that there is a region that is magnetic and that has a reasonably high dielectric constant [≈120  $(BTO)_{0.5}-(CFO)_{0.5}$ ]. High values of dielectric constant are often a good indicator of the presence of ferroelectricity.

The opposing thickness effect trend seen in Fig. 4 for magnetic and dielectric properties suggests that there is a compromise in obtaining both a high linear dielectric constant and high magnetization.

In order to confirm the dielectric and ferromagnetic properties observed here, a single composition sample with a uniform average composition of  $(BTO)_{0.45}$ – $(CFO)_{0.55}$ , for which the periods of CFO and BTO layers were  $\approx 1.4$  nm and  $\approx 1.1$  nm, respectively, was fabricated. The dielectric constant of this sample was found to be  $\approx 30$ . Figure 5 shows the SQUID magnetometer measurement result, indicating the presence of ferromagnetism in this sample.

Initial transmission electron microscopy study of the spreads indicates that when the thickness of individual layer is very thin (1-2 nm), the extent of the diffusion of BTO and CFO is such that eutectic separation seems to take place, leading to formation of separated nanoregions of BTO and CFO. This effect is expected to be less pronounced for structures with thicker individual layers ( $\geq 8 \text{ nm}$ ) in which the layered structures are expected to be maintained, in accord with the fact that no change in lattice constants was seen in the middle of the spreads for thicker individual wedge-layered samples. Further microstructural investigation and measurements to directly confirm the presence of ferroelectricity as well as the magnetoelectric effect using capacitors are currently underway.

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